

Amendments to the Specification:

The paragraph starting at page 1, line 24, is amended and now reads as follows:

-- United Kingdom patent application 2,192,968 (corresponding to United States patent application 888,595, filed July 23, 1986) is directed to comparatively large vibration amplitudes in the region of the inherent frequency of the damping system as well as to high frequency vibrations of comparatively small amplitude. For attenuating low frequencies of large amplitude, there are two volume-changeable ~~chambers~~, chambers which are connected to each other via a transfer channel as in a standard hydro bushing. Additionally, a further gas chamber for taking up high frequency vibrations of low amplitude is provided and this gas chamber is closed off with an elastic membrane, that is, here, in the acoustic range, only small amplitudes can be filtered out. A further disadvantage is that additional measures are required for damping the expanded range. The manufacture with respect to these measures is associated with additional complexity. --

The paragraph starting at page 2, line 14, is amended and now reads as follows:

-- The hydro bushing of the invention is for radially supporting a motor. The hydro bushing includes: a sleeve-shaped outer body; an inner support body spaced radially from the outer body; a spring body having two legs and being disposed between the outer body and the support body; a volume-changeable work chamber disposed between the legs of the spring body; the

volume-changeable work chamber being delimited to the outside by the sleeve-shaped outer body; at least one compensating chamber disposed laterally of the work chamber and having an elastic wall; a transfer channel interconnecting the work chamber and the compensating chamber; the chambers and the channel being filled with a low-viscous hydraulic fluid; the work chamber having an effective cross-sectional area ( $A_1$ ) and the spring body having a dynamic swell stiffness; the transfer channel having a length ( $L$ ) and a cross-sectional area ( $A_2$ ); and, the cross-sectional area ( $A_1$ ), the dynamic swell stiffness, the length ( $L$ ) and the cross-sectional area ( $A_2$ ) all being so selected that the hydro bushing has a natural or resonant frequency of approximately 130 Hz. --

The paragraph starting at page 6, line 26, is amended and now reads as follows:

-- With the construction in accordance with the invention, a dimensioning of transfer channels is achieved for the first time time, which makes it possible to place the frequency, which is relevant for the absorption, in the region of approximately 130 Hz. The relevant frequency is here also computed from the effective mass of the hydraulic liquid, which is vibration capable in the transfer channels, in combination with the dynamic swell stiffness of the spring body (the dynamic swell stiffness is given by the piston cross section  $A_1$  and the flow speed  $v_1$  present in the work chamber). --